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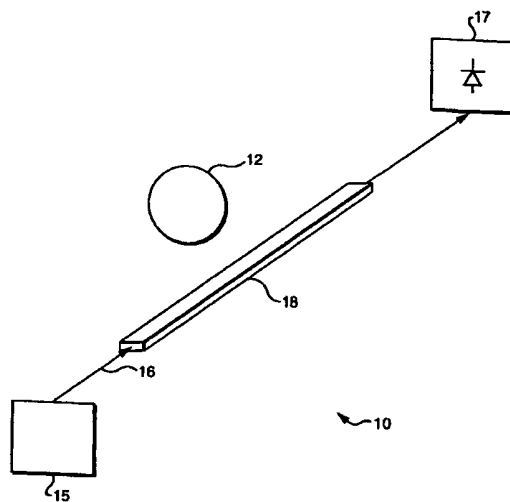
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- (71) Applicant: THE CHARLES STARK DRAPER LABORATORY, INC. [US/US]; 555 Technology Square, Cambridge, MA 02139 (US).
- (72) Inventors: TAPALIAN, Haig, Charles; 359-1F Bolivar Street, Canton, MA 02021 (US). LAINE, Juha-Pekka; Apartment 801, 534 Beacon Street, Boston, MA 02215 (US).
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[Continued on next page]

(54) Title: MICRO-OPTIC ABSORPTION SPECTROMETER



(57) Abstract: An infrared absorption spectrometer (10) features an optical microcavity (12), and a waveguide (18) that evanescently couples light into the microcavity (12). The optical resonance frequency of the microcavity (12) is tuned to coincide with an atomic or molecular resonance frequency of a selected atom or molecule. In this way, light coupled into the microcavity (12) will experience absorption in the presence of an atomic or molecular substance. The absorption causes a measurable change in the evanescent light coupling into the microcavity (12). The detection sensitivity of the spectrometer (10) is significantly increased, compared to prior art spectrometers, because of the high Q value of the microcavity (12) and the ensuing long optical path lengths of the resonant modes traveling within the microcavity (12).

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see PCT Gazette No. 41/2002 of 10 October 2002, Section II

**MICRO-OPTIC ABSORPTION SPECTROMETER****Cross-Reference to Related Applications**

This application claims the benefit of priority from U.S. Provisional Application Serial  
5 Number 60/214,383, filed June 28, 2000, entitled MICRO-OPTIC RESONATOR READOUT,  
incorporated herein by reference.

**Field of the Invention**

10 The present invention relates to optical sensors, and in particular to a high-precision,  
micro-optic absorption spectrometer.

**Background of the Invention**

During the past few years, a substantial amount of research has been performed in the  
15 field of optical microcavity physics, in order to develop high cavity-Q optical microcavity  
resonators. In general, resonant cavities that can store and recirculate electromagnetic energy at  
optical frequencies have many useful applications, including high-precision spectroscopy, signal  
processing, sensing, and filtering. Many difficulties present themselves when conventional  
planar technology, i.e. etching, is used in order to fabricate high quality optical resonators,  
20 because the surfaces must show deviations of less than about a few nanometers. Optical  
microsphere resonators, on the other hand, can have quality factors that are several orders of  
magnitude better than typical surface etched optical micro-resonators, because these  
microcavities can be shaped by natural surface tension forces during a liquid state fabrication.  
These microcavities are inexpensive, simple to fabricate, and are compatible with integrated  
25 optics.

Optical microcavity resonators have quality factors (Qs) that are higher by several orders  
of magnitude, as compared to other electromagnetic devices. Measured Qs as large at  $10^{10}$  have

been reported. The high-Q resonances encountered in these microcavities are due to whispering-gallery-modes (WGM) that are supported within the microcavities.

As a result of their small size and high cavity Q, interest has recently grown in potential applications of microcavities to fields such as electro-optics, microlaser development,  
5 measurement science, and spectroscopy. By making use of these high Q values, microspheric cavities have the potential to provide unprecedented performance in numerous applications. For example, these microspheric cavities may be useful in applications that call for ultra-narrow linewidths, long energy decay times, large energy densities, and fine sensing of environmental changes, to cite just a few examples.

10 In order for the potential of microcavity-based devices to be realized, it is necessary to couple light selectively and efficiently into the microspheres. Since the ultra-high Q values of microcavities are the result of energy that is tightly bound inside the cavity, optical energy must be coupled in and out of the high Q cavities, without negatively affecting the Q. Further, the stable integration of the microcavities with the input and output light coupling media should be  
15 achieved. Also, controlling the excitation of resonant modes within these microcavities is necessary for proper device performance, but presents a challenge for conventional waveguides.

Typically, good overall performance is gained by accessing the evanescent field in a waveguide. Also, only waveguide structures provide easy alignment and discrete, clearly defined ports. Because of cavity and waveguide mode leakage into the substrate and into the  
20 modes within the fiber cladding, power extraction from the input optical radiation has proved to be inefficient for conventional planar waveguides, however.

U.S. Patent Application Serial No. \_\_\_\_ (identified by Attorney Docket Nos. CSLL-625 and hereby incorporated by reference)(hereinafter the "CSLL-625" application) discloses a highly efficient and robust mechanism for coupling optical microcavity whispering-gallery  
25 modes into integrated optical waveguide chips. SPARROW (Stripline Pedestal Antiresonant Reflecting Waveguides) are used to achieve vertical confinement and substrate isolation through

a highly reflective stack of alternating high and low refractive index dielectric layers. Q-values of over  $10^{10}$ , and coupling efficiencies of over 98% have been observed.

SPARROW waveguide chips have the potential to integrate optical microcavities into miniaturized optical sensor systems. Because of their ability to excite resonant modes having  
5   unprecedentedly high Q-values in optical microcavities, SPARROW waveguide chips have the potential for greatly increasing the resolution and dynamic range in these sensing applications.

In particular, a significant potential application for microcavity resonator devices is chemical / biological agent sensing. Chemical sensors known in the art include MEMS (microelectromechanical systems) chemical sensors, optical waveguide-based sensors, surface  
10   plasmon resonance (SPR) chemical sensors, surface acoustic wave (SAW) chemical sensors, mass spectrometers, and IR (infrared) absorption spectrometers. Miniaturized sensors, such as prior art MEMS sensors, provide significant advantages. For example, they would be well adapted for *in situ* functioning. Also, they would be small enough to be deployed in large numbers and implemented for remote probing.

15       It is desirable to provide chemical sensors with an improved resolution, while maintaining the compact size of MEMS sensors known in the art.

### Summary of the Invention

The present invention is directed to a light absorption spectrometer, formed of a  
20   waveguide-coupled optical microcavity resonator. The present invention features the tuning of the optical resonance frequency of the microsphere, to coincide with a selected electronic or vibrational transition frequency, so that the light coupled into the microsphere will experience absorption in the presence of an atomic or molecular substance surrounding the microsphere.

An infrared absorption spectrometer constructed in accordance with the present invention  
25   includes at least one optical microcavity, and an optical waveguide for coupling light into a resonant mode of the optical microcavity. The optical waveguide has an input end and an output

end. The waveguide is adapted for transmitting optical radiation incident on the input end to the output end.

The light coupled into the optical microcavity is adapted to interact with at least one an atomic or molecular species. The atomic or molecular species may be found in a chemical substance surrounding the microcavity, and may be a fluid, by way of example. The optical microcavity is configured so that the frequency of at least one resonant mode of the optical cavity matches an electronic or vibrational transition frequency of the atomic or molecular species. In this way, optical radiation coupled into the optical microcavity and having a frequency substantially equal to the frequency of the resonant mode is absorbed by the atomic or molecular species.

Because of the high Q value and the correspondingly long optical path length of the optical microcavity, the sensitivity of the infrared absorption spectrometer of the present invention is significantly increased, as compared to the prior art.

#### Brief Description of the Drawings

Figure 1 is a schematic diagram of an infrared absorption spectrometer, constructed in accordance with the present invention.

Figure 2 illustrates a SPARROW optical waveguide, constructed in accordance with the present invention.

Figure 3 illustrates an optical waveguide constructed in accordance with the present invention, and having a Mach-Zehnder interferometric configuration.

#### Detailed Description

The present invention is directed to an infrared (IR) absorption spectrometer, formed of a waveguide-coupled optical microcavity resonator. Optical microcavities are characterized by high Q values and correspondingly long optical path lengths, allowing a significant increase in

the sensitivity of the infrared absorption spectrometer, as compared to prior art absorption spectrometers.

Figure 1 is a schematic diagram of an infrared absorption spectrometer 10, constructed in accordance with the present invention. The spectrometer 10 includes at least one optical microcavity resonator 12, and a waveguide 18 for evanescently coupling light from the waveguide 18 onto the microcavity 12. In the present invention, the optical resonance frequency of the microcavity is tuned to coincide with a vibrational resonance frequency of the interacting molecule, such that the light coupled into the microsphere will experience absorption in the presence of the chemical vapor surrounding the microsphere. An optical source 15, preferably a laser, provides a beam 16 of input radiation directed to the waveguide. A photodetector 17 detects optical radiation transmitted through the waveguide 18.

The optical microcavity 12 is a small spherical particle, disk, or ring, having dimensions of the order of microns to millimeters. The optical microcavity 12 is typically made of silica. In a preferred embodiment, the optical microcavity 12 is fabricated by surface tension shaping of the tip of freshly melted optical fiber. Melting of the tip of a silica wire or fiber may be accomplished through arcing in a fusion splicer, by means of a gas flame, or using a high-power laser (such as a CO<sub>2</sub> laser) to heat the glass. Microcavities, with diameters typically ranging from about 50 micrometers to about 500 micrometers, are obtained by this method. In the illustrated embodiment, the optical microcavity has a diameter of about 200 micrometers, although other sizes are also within the scope of the present invention.

The optical microcavity 12 is adapted to support WGMs (whispering-gallery-modes), and is thus characterized by extremely high Q values. Light incident on an input end of the waveguide and propagating therethrough is evanescently coupled onto WGM resonances supported within the optical microcavity. An evanescent wave appears whenever a light wave undergoes total internal reflection at a dielectric interface, such as the interface between the silica waveguide and the surrounding air. The evanescent portion of the waveguide mode field is the exponentially

decaying portion of the waveguide mode field, outside the relatively high index region of the waveguide. The evanescent wave decays exponentially with the distance from the surface of the waveguide core on a length scale of the order of the optical wavelength.

Evanescent coupling occurs between the waveguide and the microcavity when the  
5 wavelength of the evanescent field of the waveguide mode field matches the wavelength of a resonant WGM supported within the microcavity. In a resonant WGM, light is trapped near the surface of the microcavity by repeated total internal reflections, and travels in a circle around the microcavity near the surface of the microcavity. When WGM resonances are excited in the microcavity, light continues to circulate just inside the surface of the microcavity, with virtually  
10 no loss except for residual absorption and scattering in the dielectric. This is why extremely high Q-factors, up to over  $10^{10}$ , can be achieved in the dielectric microcavities constructed in accordance with the present invention. These very high Qs translate into very high optical path lengths, and hence increased sensitivity of the spectrometer.

In a preferred embodiment, the optical waveguide is a SPARROW (stripline pedestal  
15 anti-resonant reflective optical waveguide) waveguide. Figure 2 illustrates a SPARROW optical waveguide, constructed in accordance with the present invention. The SPARROW waveguide 110 provides an efficient and robust coupling mechanism for exciting whispering-gallery-modes in an optical microcavity 102. The SPARROW 110 includes a multi-layer, high-reflectivity dielectric stack 130 disposed on the substrate 120, and a waveguide core 140. The substrate 120  
20 is substantially planar, and in one embodiment is made of silicon.

The dielectric stack 130 is composed of alternating high ( $n_H$ ) and low ( $n_L$ ) refractive index layers 131 and 132, made of a dielectric material. As a result, the dielectric stack 130 functions as a high reflectivity dielectric mirror. The larger the number of layers 131 and 132, the higher the reflectivity of the stack 130 becomes. While the illustrated embodiment includes  
25 only one low index layer 132 disposed between two high index layers 131, the number of the layers 131 and 132 can be increased in order to increase the reflectivity of the stack 130. The



alternating layers 131 and 132 forming the dielectric stack 130 provide a cladding for the SPARROW waveguide core 140, i.e. the layers forming the stack 130 may be regarded as cladding layers.

The high reflectivity of the dielectric stack 130 permits isolation of the optical modes of the microcavity 102 and the waveguide core 140 from the waveguide cladding and the substrate. By isolating the waveguide core 140 using the high-reflectivity dielectric stack 130, the SPARROW 110 circumvents the need for obtaining low refractive index cladding materials. As shown in Figure 2, one of the high refractive index layers 131 is in contact with the substrate 120.

In one embodiment, the high refractive index layer 131 is made of Si (silicon), while the low refractive index layer 132 is made of SiO<sub>2</sub> (silica). In one embodiment, the high refractive index  $n_H$  is about 3.5, and the low refractive index  $n_L$  is about 1.45, although other refractive indices are also within the scope of the present invention. The refractive indices required for efficiently guiding light within the waveguide depend on the wavelength of optical radiation.

The waveguide core 140 is disposed on top of the dielectric stack 130, and is in contact with another one of the high refractive index layers 131. The waveguide core 140 includes an input end 142 and an output end 144, and is adapted for transmitting optical radiation incident on the input end 142 to the output end 144. In one embodiment, the waveguide core is made of silica, and is characterized by the low refractive index  $n_L$ . In a SPARROW waveguide, the waveguide mode field is essentially entirely contained within the waveguide core 140 on top of the dielectric stack 130, and is isolated from the substrate 120. The successful elimination of both the microcavity mode and the waveguide mode leakage into the substrate results in extremely high coupling efficiencies. Coupling efficiencies approaching 100% have been observed.

Figure 3 illustrates an optical waveguide constructed in accordance with the present invention, and having a Mach-Zehnder like interferometric configuration. In a Mach-Zehnder

interferometer, an incoming optical signal is split into two signals, for example at a Y-junction. Each signal enters a first and a second waveguide branch, respectively. The signals are recombined into an output waveguide, which provides a modulated optical output signal. An electric field applied to one or both of the waveguide branches causes a change in the refractive index in the applied region, corresponding to the changing amplitude of the modulating signal. The change in the index of refraction alters the speed of light in the region, resulting in a change in the delay time of the light passing through the region. The optical path length in one or both of the waveguides branches can be controlled, so that a phase difference results between the two signals when they are recombined at the output waveguide.

10 The waveguide 500 has an input end 510 and an output end 512. The interferometric waveguide 500 includes three waveguide arms 505, 506, and 507. The first arm 505 forms an input channel, and is adapted to input coupling light into the microsphere. The second arm 506 forms a drop channel, and is adapted to out-couple light from the microcavity into the waveguide. The third arm 507 is used as a reference channel, which has substantially no  
15 interaction with the microcavity. At the output end 512, light from the reference channel 507 is combined or interfered with light from the drop channel, i.e. light that has interacted with the microsphere.

The sensitivity of absorption-based sensors is proportional to the optical path length. The change in phase experienced by the resonant light and measured by the interferometer may be  
20 expressed in terms of the cavity lifetime  $\tau(d)$  of the microcavity, and the optical path difference (OPD)  $l(d)$ . The cavity lifetime  $\tau(d)$  for resonant light can be expressed as a function of the total cavity Q:

$$\tau(d) = \frac{Q(d)}{\omega}$$

25 Assuming interferometer arms of equal path length, the optical path length  $l(d)$  can be expressed

as a function of the cavity lifetime,

$$l(d) = \frac{c}{n} \tau(d) = \frac{\lambda}{2\pi n} Q(d)$$

From the equation provided above, it can be seen that high-Q microcavities provide a way to obtain the high sensitivities associated with long path lengths in a miniature sensor package. In contrast, the optical path lengths available on integrated optical chips are limited, 5 resulting in reduced sensitivity. Using fused silica microcavities as described above, optical path lengths as long as 100 m can be achieved.

In the present invention, the optical resonance frequency of the microsphere is "tuned" to coincide with a selected electronic or vibrational transition frequency such that the light coupled 10 into the microsphere will experience absorption in the presence of an atomic or molecular substance surrounding the microsphere. The result is a change in the measured light transmittance.

The technique of the present invention, when applied to IR absorption spectroscopy, takes advantage of the large absorption coefficients of molecular vibrations in the mid-IR region 15 of the electromagnetic spectrum, typically ranging from about 3  $\mu\text{m}$  to about 20  $\mu\text{m}$ . Small molecules, typically 4 atoms or less, possess strong vibrational transitions toward the lower end of the infrared spectrum. The fraction of light absorbed by a molecular sample is given by

$$I_a / I_0 = 1 - e^{-\alpha p L},$$

where  $I_a$  is the absorbed laser intensity;

20  $I_0$  is the incident laser intensity;

$\alpha$  is the absorption coefficient;

$p$  is the vapor pressure of the molecular vapor;

and  $L$  is the absorption length, i.e. optical path length.

In one embodiment, the resonant wavelength of fused silica microcavities can be shifted 25 into the mid-infrared region, by coating the microcavities with a gold nanoshell, i.e. a layer of

gold having a thickness of the order of nanometers.

In an exemplary embodiment, the infrared absorption technique described above may be implemented using methane, which has a 3.3  $\mu\text{m}$  vibrational transition. Using an optical microcavity having an optical path length of 50 cm, and an absorption measurement resolution of  
5  $10^{-6}$ , the methane detection sensitivity is approximately 100 ppt (parts per trillion).

Because of the high-Q values and ensuing large optical path lengths of microcavity resonators, the infrared absorption spectrometer disclosed in the present invention provides a significantly increased sensitivity, as compared to prior art miniature infrared absorption spectrometer. The infrared absorption spectrometer, constructed in accordance with the present  
10 invention, provides all the advantages of a compact size, in combination with its high sensitivity. The present invention may have wide ranging applications in the industry and the military, including but not limited to the fields of manufacturing process control, environmental monitoring, combustion bi-product monitoring, and chemical/biological agent sensing on the battlefield.

15 While the invention has been particularly shown and described with reference to specific preferred embodiments, it should be understood by those skilled in the art that various changes in form and detail may be made therein without departing from the spirit and scope of the invention as defined by the appended claims.

CLAIMS

1. An infrared absorption spectrometer, comprising:

A. a substrate;

B. an optical waveguide having an input end and an output end, said waveguide  
5 being adapted for transmitting optical radiation incident on said input end to said  
output end; and

C. at least one optical microcavity constructed and arranged so as to optically  
interact with light incident on said input end of said optical waveguide core, so  
that light from said waveguide core is coupled into said microcavity;

10 wherein light coupled into said optical microcavity is adapted to interact with at least one  
of an atomic and a molecular species; and

15 wherein said optical microcavity is configured so that the frequency of at least one  
resonant mode of said optical cavity matches a vibrational frequency of said at least one  
of an atomic and a molecular species, so that optical radiation coupled into said optical  
microcavity and having a frequency substantially equal to said frequency of said at least  
one resonant mode is absorbed by said at least one of an atomic and a molecular species.

20 2. An infrared absorption spectrometer according to claim 1, wherein said optical  
microcavity is disposed at a distance from said optical waveguide that is sufficiently small to  
cause the evanescent field of said optical radiation propagating through said optical waveguide to  
be optically coupled into said microcavity.

3. An infrared absorption spectrometer according to claim 2, wherein said evanescent field is characterized by frequencies substantially equal to a resonant modes of said optical microcavity.

5 4. An infrared absorption spectrometer according to claim 3, wherein at least one of said resonant modes of said optical microcavity is a whispering gallery mode.

5. An infrared absorption spectrometer according to claim 4, wherein said optical microcavity has a substantially spherical shape, and wherein the wavelengths of the whispering  
10 gallery modes of said microcavity are related to the radius  $r$  and the degree of sphericity of said substantially spherical microcavity, and are approximately given by the formula:

$$2 \pi r = n \lambda,$$

where  $n$  is a nonzero integer.

15 6. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide comprises:  
a splitter for splitting said input optical radiation into a first signal and a second signal;  
a first waveguide branch and a second waveguide branch for transmitting said first signal and said second signal, respectively; and  
20 a combiner for recombining said first signal and said second signal.

7. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide includes channels arranged in a Mach-Zehnder interferometer configuration.

25 8. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide core includes a drop channel, a throughput channel, and a reference channel, arranged

so that the optical microcavity can optically interact with both the drop channel and the throughput channel, but does not substantially optically interact with light in the reference channel.

5 9. An infrared absorption spectrometer according to claim 1, wherein said optical microcavity is selected from the group consisting of microspheres, microdisks, and microrings.

10. An infrared absorption spectrometer according to claim 1, further comprising a light source arranged to input light into said input end of said optical waveguide.

10

11. An infrared absorption spectrometer according to claim 1, further comprising at least one detector constructed and arranged so as to detect output optical radiation from said output end of said optical waveguide.

15 12. An infrared absorption spectrometer according to claim 1, wherein said optical microcavity is made of silica.

13. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide is an integrated optical chip.

20

14. An infrared absorption spectrometer according to claim 1, wherein the coupling efficiency of said evanescent field of said optical radiation coupled into said optical microcavity is from about 10% to about 98%.

25 15. An optical resonator according to claim 1, wherein said optical microcavity is fabricated by melting one end of an optical fiber.

16. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a quality factor (Q) from about  $10^5$  to about  $10^{10}$ .

5 17. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a diameter of about 50  $\mu\text{m}$  to about 500  $\mu\text{m}$ .

18. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a diameter of about 200  $\mu\text{m}$ .

10

19. An optical resonator according to claim 2, wherein said distance is less than one wavelength of said optical radiation propagating through said optical waveguide.

20. An optical resonator sensor according to claim 1, wherein said optical waveguide  
15 comprises:

(a) a multi-layer dielectric stack disposed on said substrate, said dielectric stack including alternating high and low refractive index dielectric layers;  
and

(b) a waveguide core disposed on said dielectric stack and having an input end  
20 and an output end, said waveguide core being adapted for transmitting optical radiation incident on said input end to said output end.

21. An optical resonator sensor according to claim 20, wherein one of said low refractive index layers is in contact with said substrate, and wherein one of said high refractive index layers  
25 is in contact with said waveguide core.



22. An optical resonator sensor according to claim 20, wherein said low index dielectric layer and said waveguide core comprises silica.

23. An optical resonator sensor according to claim 20, wherein said high index dielectric  
5 layer comprises silicon.

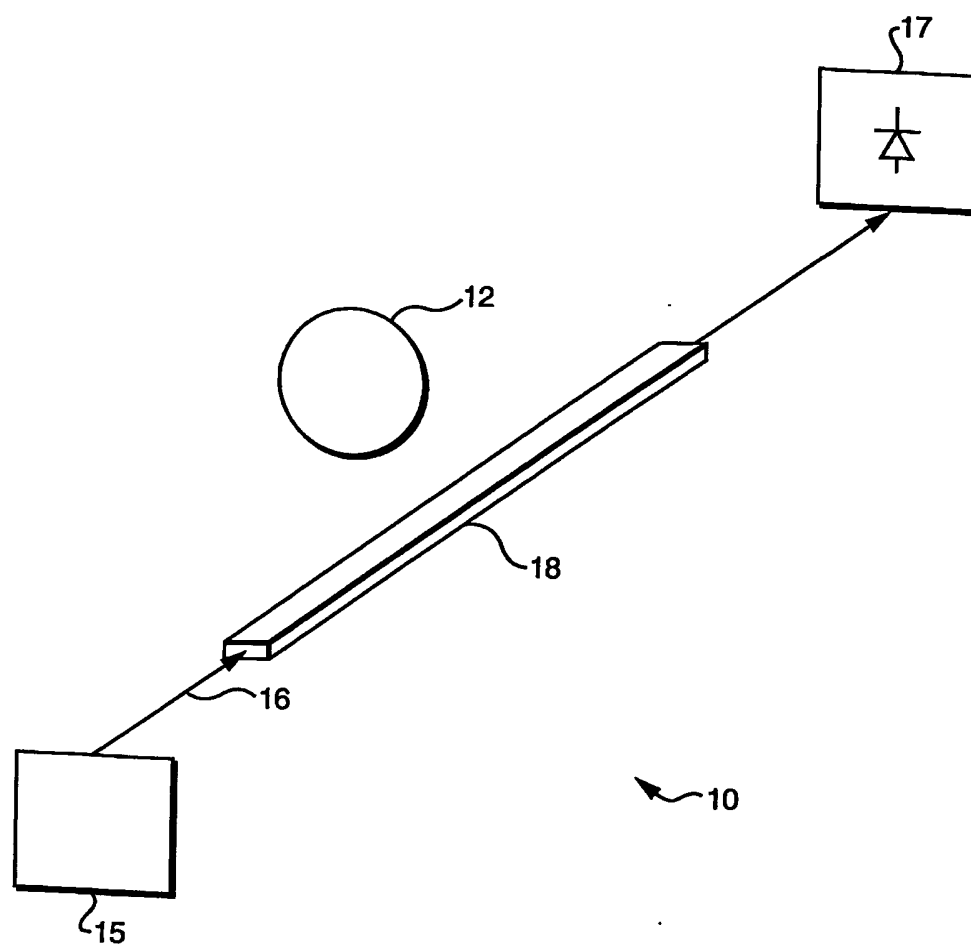


FIG. 1

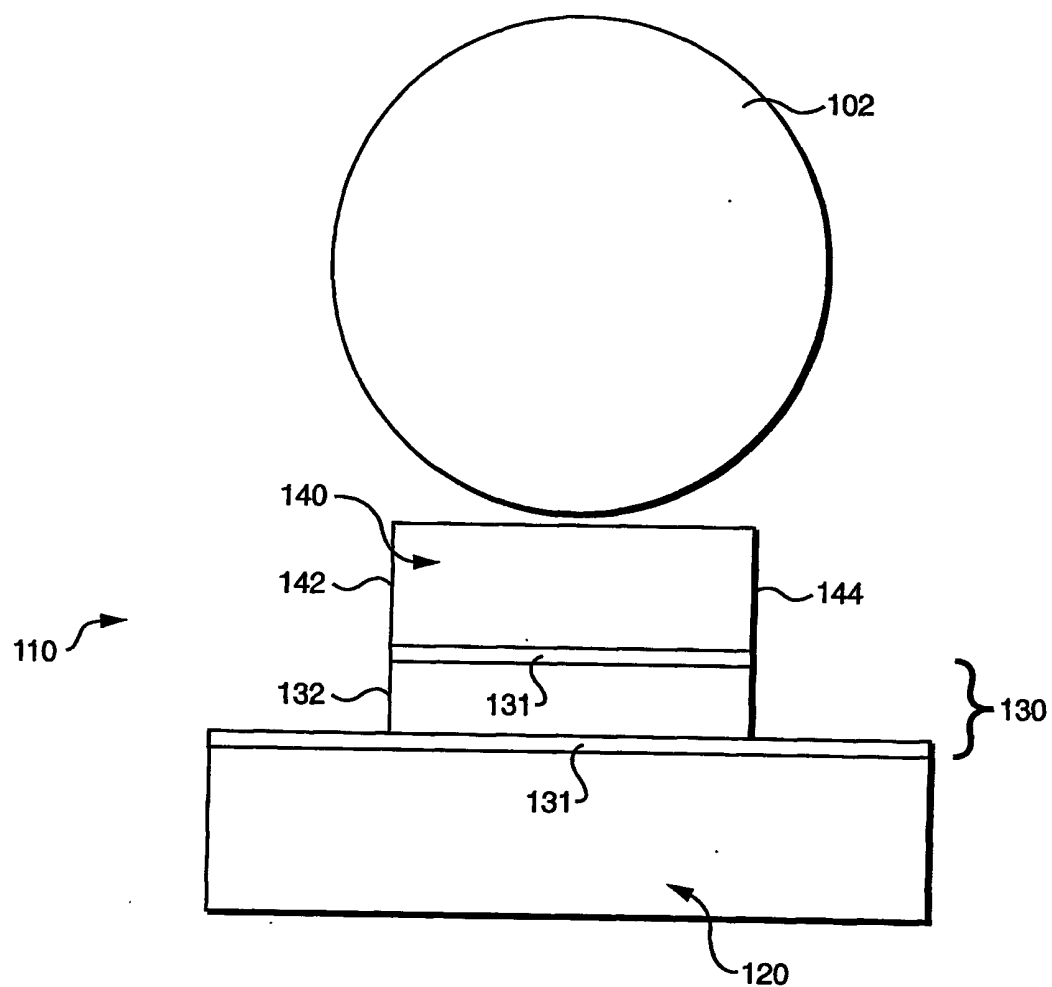


FIG. 2

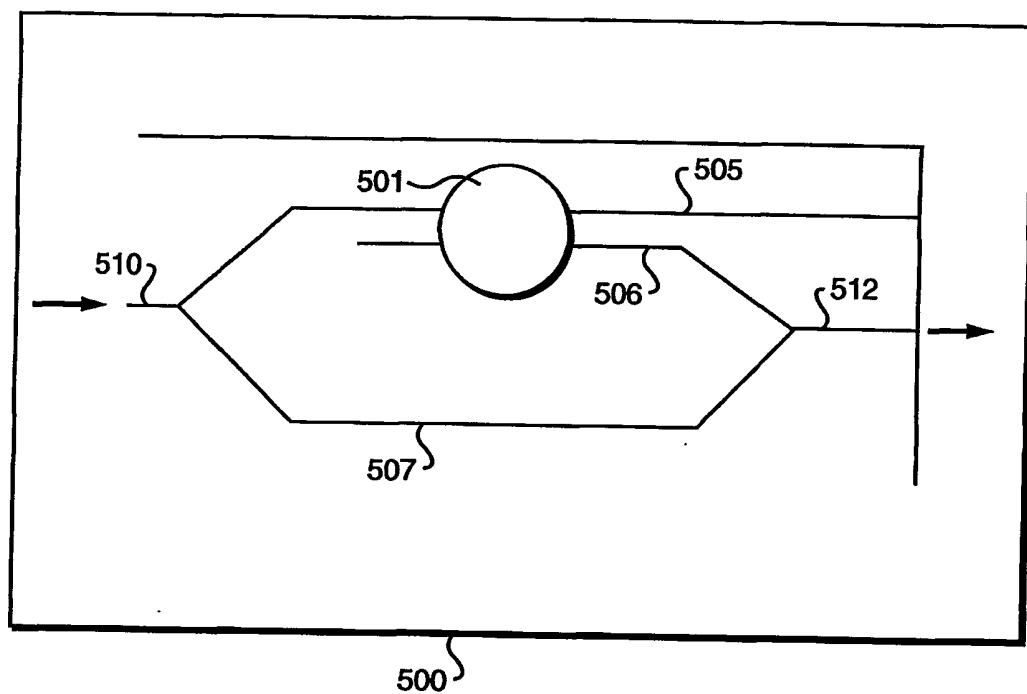


FIG. 3

**INTERNATIONAL SEARCH REPORT**  
Form PCT/ISA/210 (second sheet) (July 1998)  
FILE COPY - DO NOT MAIL

International application No.  
PCT/US01/20966

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(7) :G01N 21/65; G02B 6/12  
US CL :250/339.07

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 250/339.07; 372/74, 18; 436/172; 359/285

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
NONE

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)  
Please See Extra Sheet.

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 6,040,191 A (GROW) 21 March 2000 (21.03.2000), see entire document.	1-23
A	US 4,695,121 A (MAHAPATRA et al) 22 September 1987 (22.09.1987), see entire document.	1-23
A	US 4,807,232 A (HART et al) 21 February 1989 (21.02.1989), see entire document.	1-23
A	US 5,268,693 A (WALSH) 07 December 1993 (07.12.1993), see entire document.	1-23
A	US 5,130,843 A (HE et al) 14 July 1992 (14.07.1992), see entire document.	1-23

☐ Further documents are listed in the continuation of Box C.

☐ See patent family annex.

<p>* Special categories of cited documents:</p>	
"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E" earlier document published on or after the international filing date	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"O" document referring to an oral disclosure, use, exhibition or other means	"&" document member of the same patent family
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search  
20 SEPTEMBER 2001

Date of mailing of the international search report

**16 NOV 2001**

Facsimile No. (703) 305-3230

Authorized officer AND Telephone No. *Patricia Gabor*  
OTILIA GABOR (703) 308-4090

**INTERNATIONAL SEARCH REPORT**

Form PCT/ISA/210 (extra sheet) (July 1998)

FILE COPY - DO NOT MAIL

International application No.

PCT/US01/20966

**B. FIELDS SEARCHED**

Electronic data bases consulted (Name of data base and where practicable terms used):

USPTO WEST 2.0

search terms: spectrometer, infrared, optical waveguide, optical cavity, optical microcavity, resonant cavity, vibrational frequency, resonant mode, optical resonator

CLAIMS

250/339.07

1. An infrared absorption spectrometer, comprising:

- A. a substrate;
- B. an optical waveguide having an input end and an output end, said waveguide being adapted for transmitting optical radiation incident on said input end to said output end; and
- C. at least one optical microcavity constructed and arranged so as to optically interact with light incident on said input end of said optical waveguide core, so that light from said waveguide core is coupled into said microcavity;

10

wherein light coupled into said optical microcavity is adapted to interact with at least one of an atomic and a molecular species; and

wherein said optical microcavity is configured so that the frequency of at least one resonant mode of said optical cavity matches a vibrational frequency of said at least one of an atomic and a molecular species, so that optical radiation coupled into said optical microcavity and having a frequency substantially equal to said frequency of said at least one resonant mode is absorbed by said at least one of an atomic and a molecular species.

- 20 2. An infrared absorption spectrometer according to claim 1, wherein said optical microcavity is disposed at a distance from said optical waveguide that is sufficiently small to cause the evanescent field of said optical radiation propagating through said optical waveguide to be optically coupled into said microcavity.

3. An infrared absorption spectrometer according to claim 2, wherein said evanescent field is characterized by frequencies substantially equal to a resonant modes of said optical microcavity.

5 4. An infrared absorption spectrometer according to claim 3, wherein at least one of said resonant modes of said optical microcavity is a whispering gallery mode.

5. An infrared absorption spectrometer according to claim 4, wherein said optical microcavity has a substantially spherical shape, and wherein the wavelengths of the whispering  
10 gallery modes of said microcavity are related to the radius  $r$  and the degree of sphericity of said substantially spherical microcavity, and are approximately given by the formula:

$$2 \pi r = n \lambda,$$

where  $n$  is a nonzero integer.

15 6. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide comprises:  
a splitter for splitting said input optical radiation into a first signal and a second signal;  
a first waveguide branch and a second waveguide branch for transmitting said first signal and  
said second signal, respectively; and  
20 a combiner for recombining said first signal and said second signal.

7. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide includes channels arranged in a Mach-Zehnder interferometer configuration.

25 8. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide core includes a drop channel, a throughput channel, and a reference channel, arranged



so that the optical microcavity can optically interact with both the drop channel and the throughput channel, but does not substantially optically interact with light in the reference channel.

5 9. An infrared absorption spectrometer according to claim 1, wherein said optical microcavity is selected from the group consisting of microspheres, microdisks, and microrings.

10. An infrared absorption spectrometer according to claim 1, further comprising a light source arranged to input light into said input end of said optical waveguide.

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11. An infrared absorption spectrometer according to claim 1, further comprising at least one detector constructed and arranged so as to detect output optical radiation from said output end of said optical waveguide.

15 12. An infrared absorption spectrometer according to claim 1, wherein said optical microcavity is made of silica.

13. An infrared absorption spectrometer according to claim 1, wherein said optical waveguide is an integrated optical chip.

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14. An infrared absorption spectrometer according to claim 1, wherein the coupling efficiency of said evanescent field of said optical radiation coupled into said optical microcavity is from about 10% to about 98%.

25 15. An optical resonator according to claim 1, wherein said optical microcavity is fabricated by melting one end of an optical fiber.

16. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a quality factor (Q) from about  $10^5$  to about  $10^{10}$ .

5 17. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a diameter of about 50  $\mu\text{m}$  to about 500  $\mu\text{m}$ .

18. An optical resonator according to claim 1, wherein said optical microcavity is characterized by a diameter of about 200  $\mu\text{m}$ .

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19. An optical resonator according to claim 2, wherein said distance is less than one wavelength of said optical radiation propagating through said optical waveguide.

20. An optical resonator sensor according to claim 1, wherein said optical waveguide  
15 comprises:

- (a) a multi-layer dielectric stack disposed on said substrate, said dielectric stack including alternating high and low refractive index dielectric layers; and
- (b) a waveguide core disposed on said dielectric stack and having an input end  
20 and an output end, said waveguide core being adapted for transmitting optical radiation incident on said input end to said output end.

21. An optical resonator sensor according to claim 20, wherein one of said low refractive index layers is in contact with said substrate, and wherein one of said high refractive index layers  
25 is in contact with said waveguide core.

22. An optical resonator sensor according to claim 20, wherein said low index dielectric layer and said waveguide core comprises silica.
23. An optical resonator sensor according to claim 20, wherein said high index dielectric  
5 layer comprises silicon.